UC-434

CFP 19 1986

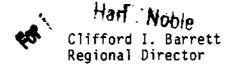
Mr. Gerald R. Zimmerman Executive Director Upper Colorado River Commission 355 South 400 East Salt Lake City, Utah 84111

Dear Mr. Zimmerman:

The final report on the methods of computing evaporation from Lake Powell is enclosed. A draft of this report was sent to you on October 30, 1984. The results of this report may be used in further studies to improve our determination of inflow to Lake Powell and bank storage. The results of these studies may help to further refine the methods of computing evaporation. Also, we hope sometime in the future to develop a procedure to determine evaporation for use in near real-time operations. This will probably involve pan evaporation measurements and weather data.

If you have any comments or questions, call Lee Morrison at 524-5573.

Sincerely yours,



Enclosure

cc: Regional Director, Boulder City, Nevada

bc: Chief, Division of Planning Technical Services, E&R Center

Attention: D-752

Power Operations Manager, Page, Arizona

bcc: LUC-434, UC-750

LMorrison:ch:9/16/86

UNITED STATES OF AMERICA DEPARTMENT OF THE INTERIOR BUREAU OF RECLAMATION

LAKE POWELL EVAPORATION

AUGUST 1986

UPPER COLORADO REGIONAL OFFICE SALT LAKE CITY, UTAH

TABLE OF CONTENTS

	PAGE
INTRODUCTION	1
METHODS OF DETERMINATION	1
PROCEDURE	2
MASS-TRANSFER METHOD	5
LAKE POWELL MEASUREMENTS	6
ADJUSTMENTS TO DATA	6
CALIBRATION COEFFICIENT	6
COMPUTATIONS	8
COMPARISON OF EVAPORATION RATES	8
GROSS EVAPORATION	8
NET EVAPORATION	8
EVAPORATION FROM PRE-RESERVOIR WATER SURFACE	14
STREAMSIDE VEGETATION	14
TERRACE EVAPOTRANSPIRATION	14
BLANEY-CRIDDLE METHOD	18
REMAINING AREA	18
RESULTS	20
RECOMMENDATIONS	20
DEFEDÉNCES	27

INTRODUCTION

j

In the early 1950's it was expected that a highly credible determination of evaporation from reservoirs in the Colorado Basin was required because of the need to divide the water between the Upper and Lower Basins according to the Colorado River Compact of 1922. The average evaporation from Colorado River Storage Project Reservoirs (Lake Powell, Flaming Gorge, Navajo, Blue Mesa, Morrow Point and Crystal) is estimated at about 600,000 acre-feet per year. About 80 percent of this is evaporated from Lake Powell. Therefore, a plan was developed to measure and collect data. Since that time it has been determined that the Upper Basin will probably not be able to develop the 7,500,000 af per year allotted by the Colorado River Compact*. Therefore, at the present time, the accuracy of the evaporation determination is not so critical. But the determination is still needed for several purposes including water use and availability studies, streamflow forecasting, and water budget studies.

This report describes and comparies several methods of determining evaporation from Lake Powell.

METHODS OF DETERMINATION

Although evaporation from a reservoir cannot be measured directly, there are several ways of determining it indirectly. One way is termed the water budget method. In this method, the inflow must equal the outflow plus or minus the change in storage. But this method cannot be applied to Lake Powell because not all of the inflow can be measured and because the bank storage cannot be measured.

Evaporation pan measurements can be used. This method is being used as a check but it has disadvantages in that pans do not account for the change in energy storage nor for advected energy.

A third way is the energy-budget method. If all of the energy entering and leaving the Lake can be measured then the energy required to balance the energy-budget is that needed for evaporation. This method is used as a check at Lake Mead for annual values. This method requires data which is expensive to obtain for periods of time shorter than 1 year. Since surface area is changing during the year it was desirable to use a method for which it was practical to obtain data to complete evaporation for periods of time shorter than a year.

Another method is based on Dalton's law which says that the rate of evaporation is a function of the differences in the vapor pressure at the water surface. This is termed the mass transfer method and the one used in this study.

*Nothing in this report is intended to interpret the provisions of the Colorado River Compact (45 Stat. 1057), the Upper Colorado River Basin Compact (63 Stat. 31), the Water Treaty of 1944 with the United Mexican States (Treaty Series 994, 59 Stat. 1219), the Decree entered by the Supreme Court of the United States in Arizona v. California et al. (379 U.S. 340), the Boulder Canyon Project Act (45 Stat. 1057), the Boulder Canyon Project Adjustment Act (54 Stat. 774; 43 U.S.C. 618a), the Colorado River Storage Project Act (70 Stat. 105.; 43 U.S.C. 620), or the Colorado River Basin Project Act (82 Stat. 885; 43 U.S.C. 1501). Pursuant to the Colorado River Basin Project Act (Public Law 90-537) of 1968.

PROCEDURE

In the late 1950's several evaporation pans were installed near Lake Powell, Flaming Gorge, and Navajo Reservoirs. Data from pans at the following locations were collected for the May-October period for 1958 through 1962 and converted into an average annual evaporation rate.

Location of Pan	Average Annual Gross Evaporation Rate in Inches
Hite	59.87
Mexican Hat	73.17
Moab	58.52
Page	69.13
Total	260.73
Average	65.18

A pan was established at Green River, Utah, but the data was not used. A pan was installed at Wahweap in 1962, but the data was not available when the average annual evaporation rate was determined.

A method was established to determine the evapo-transpiration from the prereservoir Lake Powell area and data was collected before the Lake started to fill. The amount of evaporation caused by Lake Powell was estimated by multiplying the evaporation rate (65.18 inches) by the lake area and subtracting the evapo-transpiration from the equivalent pre-reservoir area. This evaporation has been used to the present time (Table 8). The method and the computations for determining the evaporation from the equivalent pre-reservoir is in the files of the Water Operations Branch of the Upper Colorado Region.

Studies of several methods of determining evaporation had been made at Lake Hefner in Oklahoma and Lake Mead. It was decided that collecting data for the energy-budget method would be very expensive for periods of time less than I year. Since it was desirable to determine evaporation for shorter periods of time, it was decided not to use the energy-budget method. It was also desirable to make a determination independent of the pan method. Therefore, the mass-transfer method was selected.

Three rafts were constructed, instrumented, and placed at Wahweap Bay, Padre Bay, (also called Crossing-of-the-Fathers), and Bullfrog Bay as shown in Figure 1. The data was processed in the early 1970's but there was some concern as to the coefficient to use in the equation. At that time scientists from several universities were investigating several aspects of Lake Powell. The studies, sponsored by the National Science Foundation, were named the Lake Powell Research Project. A cooperative agreement was made to make an evaporation study as part of their water budget analysis. The Bureau furnished instruments and another raft which was installed at Hite. The Bureau participated in this to obtain data to calibrate a mass-transfer coefficient for the data we had collected. New cassette recorders and sensors were installed on the rafts along with the old equipment which was still being used. Data was collected for about 2 years and analyzed by the energy-budget and mass-transfer methods and compared with pan measurements.

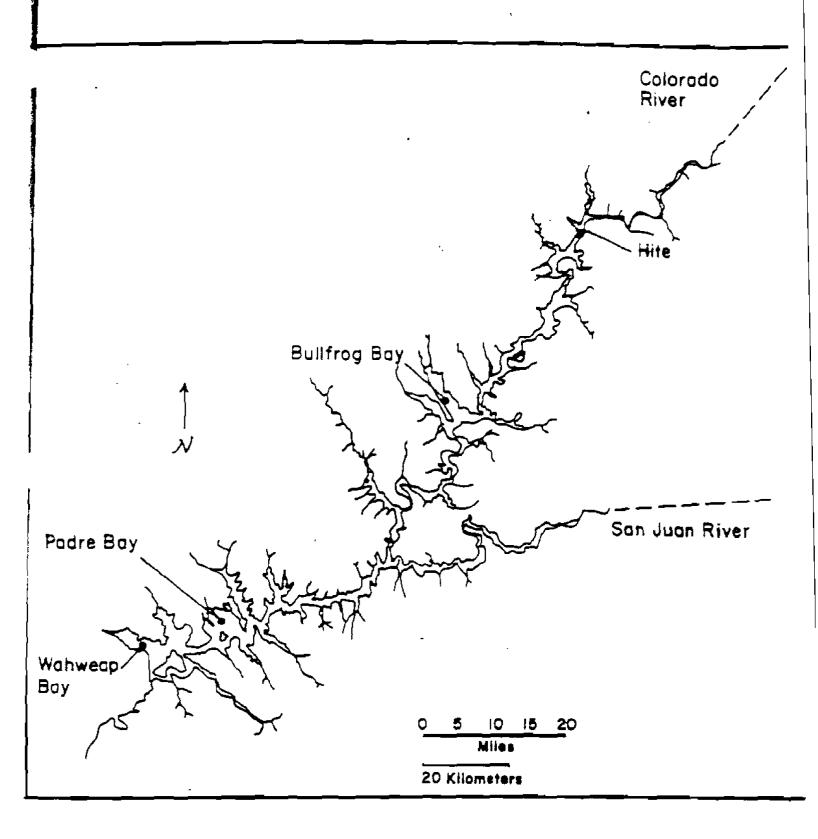


Figure 1: Locations of Data Collection System Rafts for Evaporation Study of Lake Powell

MASS TRANSFER METHOD

The following is a brief description of the mass-transfer method. A simple example of the same type as the Lake Hefner quasi-empirical equation is

$$\mathsf{E} = \mathsf{Nu}(\mathsf{e}_{\mathsf{O}} - \mathsf{e}_{\mathsf{a}}), \tag{1}$$

in which E=evaporation, in inches per day;

N=a coefficient of proportionality, hereafter called the masstransfer coefficient;

u=wind speed, in miles per hour, at some height above the water surface; a numerical subscript, if used, indicates the height in meters;

e_o=saturation vapor pressure in millibars, corresponding to the temperature of the water surface;

ea=vapor pressure of the air, in millibars; a numerical subscript, if used, indicates the height in meters.

Nearly all the mass-transfer equations to be found in the literature have one thing in common: evaporation is considered to be proportional to the product of the wind speed, u, and the vapor-pressure difference, \mathbf{e}_0 - \mathbf{e}_a . In a few equations, the wind speed, u, has an exponent, usually less than unity.

The mass-transfer coefficient, N, represents a combination of many variables in the published mass-transfer equations. Among these are the manner of the variation of wind with height, the size of the lake, the roughness of the water surface, atmospheric stability, barometric pressure, and density and kinematic viscosity of the air.

The following mass-transfer equation was developed for Lake Mead and used to make monthly determinations of evaporation rates. These determinations have been checked on an annual basis by the energy-budget and panevaporation methods.

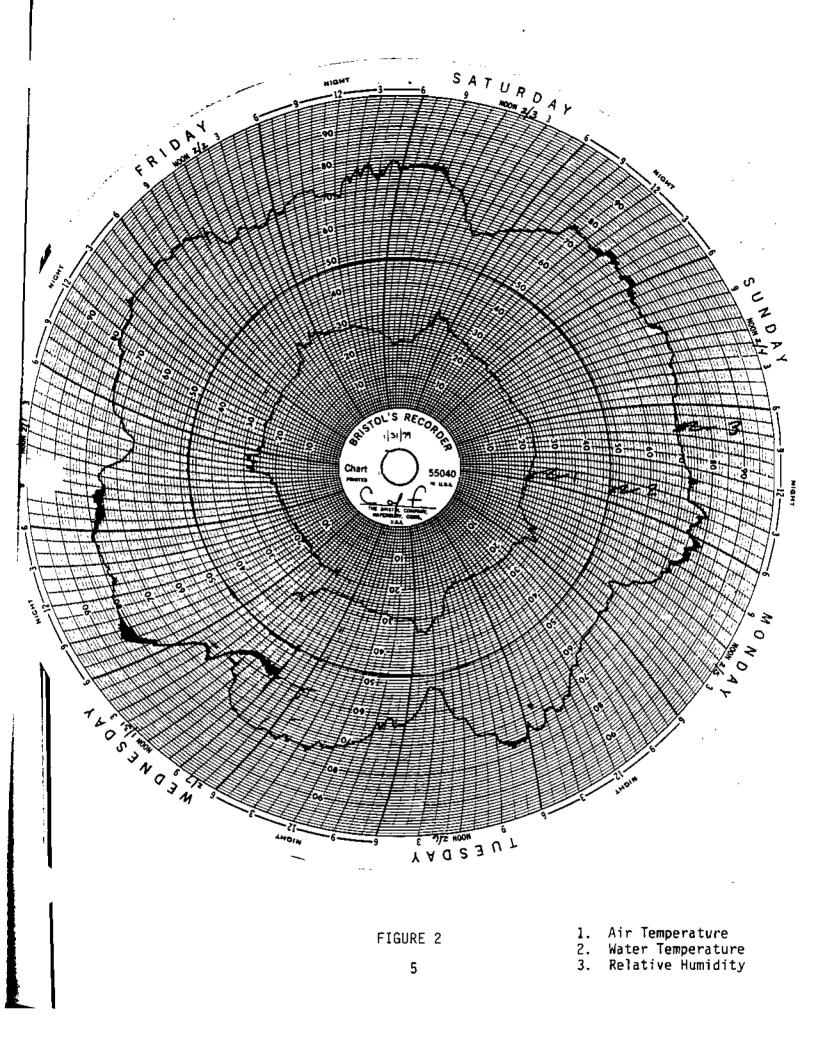
$$E = 2.65 \times 10^{-3} U_2 (e_0 - e_2)$$
 (2)

E = evaporation in inches per day.

U2= is wind speed in knots.

e_o= is saturation vapor pressure at the temperature of the water surface.

e2= is the vapor pressure of the air computed in millibars at 2
meters above the water surface.



LAKE POWELL MEASUREMENTS

The following data was collected from each of the three rafts; water surface temperature, air temperature, and relative humidity. The wind was measured by an anemometer placed two meters above the water surface. The anemometers were read once each week. At each of the three rafts, water surface temperature, air temperature, and relative humidity were recorded on 7 day circular charts as shown in Figure 2. Wind was measured and recorded by anemometers placed 2 meters above the water surface which were read once each week. The data was manually read and recorded on the form shown in Figure 3.

ADJUSTMENTS TO DATA

The wind run was required on a daily basis but the raft anemometers were only read weekly on the rafts. Therefore, the daily wind run from anomemeters at the Wahweap Marina and Page were used to pro rate the weekly raft wind run readings for each day.

Some of the data was not recorded or was obviously wrong. Therefore, methods were developed to estimate missing data either by interpolation, observing trends before and after the missing data, or by correlation with data from other rafts. Wind has a large effect on evaporation and is highly variable. Therefore, a procedure was developed to estimate missing wind data using a hierarchy of options starting with the most preferred method. This procedure is explained in the files of the Water Operations Branch. Other details and computer printouts are also available in these files.

CALIBRATION OF COEFFICIENT

The evaporation rate as determined by the Lake Powell Research Project (LPRP) was used to calibrate a mass-transfer coefficient. For those days in 1974 when there was concurrent data as collected by the LPRP instruments and Bureau instruments a regression analysis was made for each of the three data stations. Thus there were 295 data sets at Wahweap Bay, 143 data sets at Bullfrog Bay and 133 data sets at Padre Bay. The regression coefficients were; .53 at Wahweap; .72 at Padre Bay, and .55 at Bullfrog Bay. These coefficients are not very high mainly because of the determined distribution of wind data. If the regression analysis were done for weekly or longer periods, the regression coefficients would be much higher. A comparison of monthly rates is shown in Table 1. From the regression analysis a mass transfer coefficient of 3.27 was determined and used in equation (3).

DATA FOR CO: A' BY MAS

									1 4	KF	P.	we	- , ,		L									ΕΑΙ	_						_				CRO	วร
	1													-		ΑI	R	TEI	MP.		WA'	TER	н	UM	DIT	Υ	ΔN	EM	ОМ	ETI	ΕR	_	Α		TEM	_
40.		DΑ	YY			AF						TIC			_	MAX	€.	П	MII	٧.	TΕ	MP	М.	AX.	м	IN.	1	RE A	ΔDI	NG		١-,	4.6.	,	м	-
1 2	2	3	4	5	6	7	8	9	10) [1	!2	13	14	15	16	17	18	119	2 (21	22	23	2 4	25	126	27	28	29	30	3	32	33	34	35	36
									•				Į			ĺ															-				П	
Ì	T						i	T	i	-			ļ			_	_	\vdash							†			-			-		-		H	_
:	Ţ						Ī	Τ	İ				į					Г							✝		Ι-					_			H	_
1	T			Г	,		Ť.	T	- -	T								T		1		_		 	t—	-				-					├	_
	\top	\neg			i	+	<u> </u>	†	1		\top		ij					\vdash	Ť	T	H		\vdash	╁	 		\vdash		-			\vdash	_	-	H	
i	Ť	_			-	1	†	T	 	+	_							H	\vdash	 				<u> </u>	t—	 	-			\vdash		—		L	┟╌╁	_
į	\dagger				:	\vdash	į	T	;	Ť	+	\top						\vdash		ļ					 —		\vdash	-		<u> </u>						_
+	\dagger				<u> </u>		i	†	Ť	Ť	\top	\top	_					\vdash	-	Ì				.	 	 -						_				_
	†				i	+ "	;	\vdash	i		$^{+}$	+	+						 	\vdash				1	-	-	\vdash		_	<u> </u>		_		\vdash	-	_
\dagger	+				i	 	 	╁	+	t	+	+	\dashv			_	-	\vdash	!	 	 				-	:	├-								\vdash	_
t	+	+	\dashv			+	 -	†	-	+	+	+	\dashv		-	_		\vdash		-	H				 		\vdash	\vdash	_						\vdash	_
+	+	\dashv	\dashv			+	Ť	+	+	+	+	+	\dashv		_			\vdash		-			-			\vdash	_			-					$\vdash \vdash$	
+	+	\dashv	\dashv			+	+	+	+	<u></u>	-	\dashv	-+				_	\vdash			$\vdash \vdash$		\vdash		-			-						\blacksquare		
╁	╁	-	-			╁	 -	-	+	•	+	+	\dashv					┢	1	<u> </u>		_			-										-	_
+-	十	+				\vdash	+	╁	+	+	+-	+		ᅱ	_			\vdash		<u> </u>	\vdash				-											
+	╁	\dashv	-			\vdash	<u>;</u> ;	┼	+-	+	+	+	+	\dashv				-				-		_		Ш								_	_	_
+	+	+		_		┝.		┼-	+-	+-	-	+	\dashv	\dashv				\vdash				-														
╁	+	\dashv	ᅱ				_	\vdash	+	+-	+		+	\dashv	_			_	_		 	\dashv			H						\Box				_	
+	+	\dashv	\dashv	_		_	<u> </u> 	┝	+	+	+	+	1	\dashv				┝	:		<u> </u>	\dashv							_						\dashv	
 	┩╌					 	-	⊢	-	+	+	\rightarrow	4	\dashv				<u> </u>	<u> </u>	<u> </u>	,	_									_					
┿	-	+	\dashv					╀	+	+	+	 	4							<u> </u>		-4							_		_					
╁	+	<u>;</u>	\dashv	- 1			-	┞	_	+	+	+	\dashv	4						-	<u> </u>		_					1		<u></u>	_					
╀	╀	+	\dashv	-		_		┝	+-	-		+	_		_				-	<u> </u>	<u> </u>		_		_	_	Į	_			_		į	_		_,
!	╀	+	_	_			<u>!</u>	ļ.	\perp	ļ	-	4	4	_				<u> </u>			_!				\Box	\Box		_								_
·	+	+	4	_		! } -	 	ļ	 	Ļ	\downarrow	+	4	_				_		ļ	-		\perp												\perp	
-	╀.	4	_	į		i	!	L	!	<u> </u>	\downarrow	4		_							j													\bot		<u>;</u>
\perp	╄	\downarrow	_	_				┡	<u> </u> _	\perp	-	4								L.			_				_									
ļ	╄	4	_	_			_	Ļ.	 	\perp	\perp	\perp	1	_						Щ.			_				Ì	!								j
L	╀	4		<u> </u>			<u> </u>	L	\perp	\perp	!		_	_					L.,			┙			ļ				ĺ							- i
_	┸	_	_				!			<u> </u>															į			Ţ			╗			ľ		_
	┸	_					<u> </u>	L	$oxed{}$		Ĺ										i				i						コ		\neg	7	\top	
	L	\perp					<u>i </u>	L	<u> </u>					╛	-										į			;		j			1	T	\top	
<u> </u>	L		_								Ĺ			\perp	j						į	\Box			i			Ī			ヿ		T	丁		_
_	L	_[\Box	ĺ																								i	\neg	\dashv	\dashv	\dashv	\dashv	7	\top	_
	\perp	ļ	\perp	ļ		İ							j				_]						-	_]					1	1	\dashv	\dashv	-	\neg		-
						i								\Box								\exists			;	\dashv		+	1	\top	寸	_	\dashv	\dashv	7	7
	Ι	Ţ												\dashv			1				-	\dashv	\neg	1		\dashv	\dashv	_	_	\dashv	\dashv	\dashv	_	一	+	_
	Γ					i L			ļ					\dashv			寸					7		1	i	\dashv		\dashv	_	\dashv	\dagger	\dashv	+	十	1	_
	Т		7	\Box					Ţ			i	ļ	1	\neg	j	ヿ					7	\dashv		\dashv	_	\dashv	\dashv		\dashv		-+	\dashv	-†	7	_

COMPUTATION OF EVAPORATION AT LAKE POWELL M/ ^-TRANSFER METHOD

WATER AND POWER RES DIVISION OF WATER AND RESERVOIR REGULA

							ATH						L] [[_	3IN						Р	ΔG		WAI					
EMP.	_		ATER									ER			RT							ı Mı									/ I N I		l	INE				
MIN			EMP							ADI				AX			4 I N					x.				RE/					ILE			LE				
5 36	37	3	839	40	41	42	43	44	45	46	47	48	49	50	5 I	52	53	54	55	56	57	58	59	60	61	62	163	64	65	66	67	68	69	70	71	72	73	741
- [į									
7_		Ţ		Π																									Ì	Π								
Ī					[T																[Ĭ									
		Τ				T -		<u> </u>	1					<u> </u>											_				Ì							-		
1	T	T	\top	T	 -	1											<u> </u>		П										 	1		<u> </u>					_	7
+		T	+	†		┪		_		+						_	-								<u> </u>		_	<u></u>	İ	† -			H				-	+
7	i	t		† -		H	\vdash	t			_		1		_				<u> </u>	-			\vdash		┢				-							\dashv		
\top	-	╁╴	+	t	i	╁╴	 	t−		t			_	-		┢				<u> </u>			┪					_		┢							- 	
	┼-	╁╴	+	\vdash	┼-	┢		 	┤	╁	 		┝									-	┢		├-				├-	┢						-		-
-	 	╁-	+	\vdash	\vdash	\vdash	 	\vdash	 	+			├		ļ				\vdash		Н		Η.		 		 -		 	\vdash		-	\vdash			-		+
+	 	+-	-	-	-	\vdash		-	\vdash	-			-						H		Н	\vdash	\vdash		\vdash					\vdash		-	┞─┤				<u> </u>	\dashv
+	┼-	+-	┿-	╁	 	\vdash	<u> </u>	\vdash	\vdash		-		\vdash	\vdash	_		<u> </u>		\vdash		\vdash	<u> </u>			\vdash	_	<u> </u>	ļ	-	\vdash	-		\vdash	_			+	
_	-	+	+	├		\vdash	\vdash	\vdash	\vdash	+-	-	 				\vdash	_		\vdash		\vdash	-			 		<u> </u>		ļ	\vdash	-		┝┼					-
-	+	+-	+	╀	-	\vdash	\vdash	⊢	-	 	-					<u> </u>		_	\vdash		\vdash		\vdash		\vdash				ļ. <u>.</u>	├ ─	<u> </u>	-	$\vdash\vdash$					
_	╀	╁╌	┽—	╀	+	\vdash		⊢		-		 	├	 	ļ	<u> </u>	ļ <u> </u>	-	⊢⊦		\vdash		\vdash		\vdash				<u> </u>	⊢	 —		┝╌┼	1		_	_	<u> </u> -
_ '		╄	┿.	╁┈	 	┡	<u> </u>	<u> </u>		↓_	ļ	-		<u> </u>			ļ	_	<u> </u>				L				<u> </u>	ļ. <u>. </u>	!	<u> </u>					_			
_	_	╀.	<u> </u>	ļ		┡		<u> </u>	<u> </u>	↓	ļ ∔-—	<u> </u>	ļ	<u> </u>			ļ	<u> </u>	-			<u> </u>	Ļ		<u> </u>			<u> </u>	į ī	<u> </u>			L ,			_	_ ;	_
	ļ	1	_	╙		╙		<u> </u>	\vdash	 			<u> </u>					<u> </u>	Ш	<u> </u>	_	ļ,	ļ		· ·	<u> </u>				Ļ	1						\dashv	
\perp		╽.	1	ــــــــــــــــــــــــــــــــــــــ		L		L_	1	!	<u> </u>		<u> </u>			<u> </u>	<u> </u>		Ш	<u> </u>			╙							Ļ		,						
				L			L_								<u></u> _																					_		į
	ļ -			L		L	<u> </u>			<u> </u>		<u> </u>	ļ			<u> </u>		-	Ш			<u> </u>							<u> </u>									1
						L_			<u> </u>						<u>_</u> _											Ĺ				<u> </u>								_ [
		L			<u>.</u>				<u>i</u>		<u>L</u>										Ш		_		L					L							i	
				1			!			J													Ĺ.						<u> </u>		¦ i			Ī	I		ĺ	Ţ
\Box		Т	Ţ		•												Ĺ	ĺ		L			Ĺ	[Г				Ī				- ;
		T		Π			Ī		Γ														L			i												一
	T	T	1																l "												_				_			
	1	1							İ	Ī					_																						Î	\neg
	†	1							Π	i									Γ								i		·				\Box			7		_†
	 	T	_	t	Ť	†		t	1	+		\vdash	<u> </u>						Г								ı i			<u> </u>			-	_		\exists		- +
+	†	†-	\top			H			i	1-			ऻ	1									Г		-					┢			\exists		\neg			-+
	T	十	$\overline{1}$	†	i	\vdash		╁┈	†-	1			-															_	i	1			_		_	\neg	-	\top
	+-	+	+	t		t	 	\vdash	H	-								-					T	_						<u> </u>			\dashv	寸	-1	\dashv	\dashv	
	+	+		+	 	 -	 	╂	+	+	 		\vdash	 		-	- -						\vdash	-	┢		_			-			\sqcap	-	十	-+	-	\dashv
+	+-	†-	+	+-	+	H	 	\vdash	+	+	+-	\vdash	\vdash			 	'	\vdash	T			 	-						-		<u> </u>		\dashv		+	-	_ <u>-</u> !	+
- -	+	十		+	!	+-	+	t	\vdash	+			\vdash	 	 	├-	1		T		 		F	-						H		\dashv	+	_	┪	-+	+	
 	+-	╀	+	\vdash	1	+-	\vdash	+	+	+	-		\vdash		-	-		-	\vdash		\vdash			-					_	\vdash		-	\dashv		\dashv	-	\dashv	-
i	· -	+-	-	+	╀-	╁		\vdash	1	+	-	-	 	<u> </u>	 		\vdash	+	\vdash	_	\vdash	 	⊢	 -	 - -	_			-	\vdash		\dashv	+	\dashv	\dashv	_	\perp	\dashv
_		+	+	╀	-	\vdash	1	╂-	-	+	\vdash	╁	L	<u> </u>		\vdash	-	-	├				┢	ļ. <u> </u>	-					-		\dashv		-+		+		+
Щ.		_		L	1	<u> </u>			<u> </u>	1	1	1	ــــــــــــــــــــــــــــــــــــــ	<u> </u>	_	<u>. </u>		<u> </u>		:	L		<u></u>	L	 -		<u></u>		ļ	L.		4		\dashv			<u> </u>	
															ľ	Y:									/درا	ATE								- [СН	EC	K E [, .

OF EVAPORATION ELL ? "THOD

WATER AND POWER RESOURCES SERVICE
DIVISION OF WATER AND LAND OPERATIONS
RESERVOIR REGULATION BRANCH

Ή	ER	s		_	_						вι	JLL	FR	OG		3 A S	SIN		_	_	_			AG	F	WΔ	HW F	AP								_	\neg
٦	ΑN	EM	ОМ	ETE	₹R		A١	RT	EΜ	P.		WA	ΓER	н	UMI	011	ſΥ	AN	ΕM	ОМ	ĒΤ	ER	W	/ I N I	n	l w	INT	ו ר]
\neg	ş	RE/	IQ#	NG			IA X	ί.	N	1 I N		ΤE	MR	M A	١x.	МІ	N.		REA	A D I	NG	- '	М	ILE	S	м	ILE	:s									
3.	44	45	46	47	148	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76.	77	78	79	80
٦									(T																ļ .								Ī				
			1		1				┌╴		_			_			ĺ	┞╴			_				 							-			\dashv	\dashv	ᅥ
٦						Γ												Γ		Γ								!					1		_		一
٦	_	-				t —											├ ─	-			_					<u> </u>	_		-				_		- +	\neg	
1			_		i		1-		l	_		! —				Г					_		\vdash		 								 		寸	寸	
7	_		\top	 	_	┞	<u> </u>	_	ऻ		_	i -				┢	1	┞╴	_	\vdash		<u> </u>			<u> </u>						_	- 1	\dashv		_	一	\neg
					-	-		<u> </u>			-						Т	-		 	_	-			<u> </u>	-				-	\neg			_		7	一
┪	_					t –		<u> </u>						┍		Г	 	┢			_	ļ —			 										7	\dashv	
┪		1	┼-	\vdash			-				-	┞		-	\vdash		İ	-		_		-				Н				+			-	_	\dashv	\dashv	\dashv
4			\top			\vdash	I^-	<u> </u>	-	-	_					\vdash	†	 	_		$\overline{}$		Г		†					j				\dashv	+	1	\dashv
7		-	+	 		\vdash	 	\vdash	┌┈					Ι-		 	\vdash	一			-	-		 		Н						H	-+	-	-+	\dashv	\dashv
-	_		+	<u> </u>		 		 -				├ -		-		\vdash		\vdash		i			H			 	-			- i			\dashv	\dashv			\dashv
\exists	<u> </u>		+-	-		1-	一		H			 -		-	-	\vdash	 	┢	<u> </u>		-		-		 	\vdash	-		 - 				-+	-+	\dashv	-	-∤
+		<u> </u>	T		\vdash	\vdash	-		-		-				 	\vdash	 	 	-			 		ĺ	 	H	-		٠	- i	_		- +		\dashv	-+	၂
-		-	+	 	1			 - -	H	-	-		$\vdash \neg$		-	-	\vdash	┢	 	İΠ		L					_			\dashv	_			\dashv		\dashv	ᅥ
-	H		· —	 		╁				<u> </u>	_	├╌	<u> </u>	-		_	 -	┢	 		_			_	, 	-		<u> </u>		<u>_</u>	_		\dashv		-+	\dashv	一
+	-		. —		┼	├	├-		\vdash	┝	_	├		-		├-				1		İ	١			\vdash	_	\vdash		\dashv		┝━┤			-	{	\dashv
+		-	+	 		┢	├—		╁╌			-	<u> </u>			-	 	├-		 -		 			H				<u></u>	- {				-		\dashv	\dashv
\dashv	-	<u> </u>	\vdash	┼╌	 			 	\vdash	<u> </u>						┝	├-	-				<u> </u>	\vdash		 	\vdash		-		\dashv			-+		-+	\dashv	一
4		-	-		├	\vdash		-	┢╌	-		-		┝	-	┝	┥	┝		 		-	<u> </u>	Ĺ		Н	<u> </u>		_ ;	-+			\dashv	-+	\rightarrow	\longrightarrow	긕
4	-		┼─	-	 - -		├-	-	╁─	 -			<u></u>			├	<u>:</u> —	<u> </u>	<u> </u>	<u> </u>			Н]		\vdash	-	i l	_		-		\dashv		\dashv	-+	
-			⊢	-	-	┝	ļ <u>.</u>		╁┈		 - -	-	├─-	\vdash	-	┝	╁ -	├	<u> </u>	<u>-</u> -		 -			$\overline{}$	\vdash							-	-+	\dashv	\dashv	{
-		_	+	<u> </u>		├-		 -	H			-	ļ.—	\vdash		H	 	_	-		_		\vdash	<u> </u>	-		_		_					-		ᆉ	{
4	-	!	┿	<u> </u>		 		├—	}	Ļ-	 	 		┝		┝	 	-		-			Hi	-	<u>i</u>	H	_	<u> </u>					-	\dashv	$-\dot{+}$	\dashv	\dashv
4		_	 -	 	-	┝	-		┢	<u> </u>	_	\vdash	<u> </u>	-		-	├	H	_	-				_	<u> </u>	┡╌┤			—		_		\rightarrow	-+	-	-+	
4		<u>[</u>	-	 	_		├─		┼─				├-	 -		-	+-	├ ─		}				-	\vdash	┝╼		\vdash					-		-	\dashv	ᅱ
-	_		 	<u> </u>	┢	}		 - -	\vdash	}		⊢		⊢	<u> </u>	-		 	<u>L</u>	-		-		<u> </u>					\dashv	-	_		-	{			1
لـ	<u> </u>		┿-	-	\vdash	 —	-	├—	\vdash			┝╌		\vdash	 	┝	├	├		!		_	H		\vdash	Н		\dashv	4			-	\dashv		-+	\rightarrow	ᅱ
_			┼—	 	<u> </u>		 - -		 	<u> </u>		<u> </u>				┞	├ -					_						\dashv									
-	<u> </u>	<u> </u>	-	┼-	 	\vdash	\vdash		╁		-	\vdash		\vdash	\vdash	\vdash	 	 		<u> </u>			Щ	_	\vdash	Н		\vdash		 }				\dashv		\dashv	긕
-		_	-	ļ	!	├ -		-	}	 -	-		—	 	├─	-	 	┞╌					-		Н				{				-	-+	+	\dashv	{
-	├-	-	┼	-	\vdash	\vdash	<u> </u>		├	├—			ļ	┝	-	-	 	├					\vdash	_	-	\vdash		\vdash		-+				-	\dashv	\dashv	ᅴ
-	\vdash	_	\vdash		┼—	├	├ -	 	├	 	_	⊢	-	 	-		· -	├-		1	_	\vdash	\vdash	_	\vdash	$\vdash \vdash$		-- $+$	\dashv			닉	\dashv	\dashv	-+	-+	\dashv
7	\vdash	 	1	╀	-	-	-		 —		<u> </u>	- -		\vdash		\vdash	├	 	 	-			\vdash		\vdash	\vdash								-+		\dashv	\dashv
-	-	<u>:</u>	┼	↓_	1	├-	-	 - -	 	 -		\vdash	<u>'</u>	-	<u> </u>	-	 - -	-	<u> </u>	\vdash	<u> </u>		Н		\vdash	\vdash					_{	-	+	-	}	-+	ᅱ
-	<u> </u> _	!	 -	_		1		\vdash	\vdash	 	-	 		├-	 	\vdash	<u>!</u>	- -		_		H	$\left \cdot \right $		┝╌┤	$\vdash \vdash$		\dashv	-	+			 +	\dashv	\dashv	\dashv	4
-	<u> </u>	<u> </u>	_	-	<u> </u>	L	<u> </u>	-	┞-	-	ــ	}-	 	├	<u> </u>	 —	┼	 	<u> </u>	H			$\vdash \vdash$		\vdash			\dashv		\rightarrow			\dashv	\dashv			_
	L		_	 	 	 	\vdash		╀	-	 	ļ		-	├-	├ -	┼	<u> </u>	_	<u> </u>		\vdash		_	╁╼┤	$\vdash \vdash$		\dashv					- -∤	\dashv	-+	\dashv	
	_		ı		<u>L_</u>	<u> </u>		 		<u> </u>]		_	L	<u>i</u>	L,	Ц_	<u> </u>	<u>_</u>	<u>. </u>										2000							4
								B	Υ:										TE	•					_			LH	EC	KE	<i>)</i> :						
-																																					

COMPUTATIONS

Equation (3) was used to compute a daily evaporation rate. It was developed from equation (2) which was developed specifically for Lake Mead.

$$E = 3.27 \times 10^{-3} u(e_0 - 0.005(H_{max} + H_{min})e_{as})$$
 (3)

Where

E = evaporation in inches per day

u = average wind speed in miles per hour

Hmax = maximum relative humidity as percentage

H_{min} = minimum relative humidity as a percentage

 e_{as} = saturation vapor pressure in millibars at average daily air temperature.

The vapor pressure of the air is approximated by multiplying the average daily humidity by the saturation vapor pressure at the average daily air temperature. Thus the .005 in the equation is from dividing by 100 to convert from percentage and dividing by 2 to get an average. The computations were done by a computer program termed EVAP. The daily evaporation rates were totaled for each month. They are shown in Table 2.

COMPARISON OF EVAPORATION RATES

Table 3 is pan evaporation as measured at Wahweap. Table 4 is the Lake Powell evaporation rate in inches from the adjusted class A pan at Wahweap Arizona. This adjustment is described in Lake Powell Research Bulletin Number 48. The average annual evaporation rate for the evaporation pan method was 69.44 inches for the 1962-1975 period while the rate for the mass-transfer method was 68.32 inches for the same period.

GROSS EVAPORATION

The gross evaporation is computed by multiplying the lake surface area by the evaporation rate in Table 2. This is shown in Table 5 and column (1) of Table 8.

NET EVAPORATION

Net evaporation which is the amount of increased evaporation caused by the reservoir is needed for some purposes. It is needed to establish water supply data that is homogeneous for the period before and after Lake Powell started to fill. It is also needed to determine depletion.

Net evaporation is determined by subtracting from the gross evaporation the evapotranspiration that would have occured from the reservoir basin if the

TABLE 1 COMPARATIVE EVAPORATION RATES FOR CALIBRATION PERIOD

	Jan	Jan Feb	Mar	Apr	May	June	July	Aug	Sept	Oct	Š,	Dec
Wahweap LPRP 1/ Bay Bureau 2/	3.09	3.09 3.75 4.76 4.18	3.26	4.70 5.29	5.52 5.83	7.73	7.98	9.11		5.27	4.88 5.26	4.59
Padre LPRP $1/8$ Bay Bureau $2/8$	3.65	3.65 3.15 4.13 4.17 4.17 3.32	4.13	3 5.72 7 3.15 4	7.61	8.17	8.36	7.73	5.67	3.49	4.44	
Bullfrog Bay Bureau <u>2</u> /	3.04	3.04 2.35 2.61	2.61	3.84	5.24 5.65	5.65	8.46	8.36	7.54	5.44	5.44 3.95	3.96
Adjusted Pan 3/				4.66	5.55 7.85	7.85	8.24	8.89		5,65	5.65 4.74	

1/ As computed by Lake Powell Research Project $\overline{2}/$ As computed using equation (3) using mass-transfer coefficient derived by regression analysis. $\overline{3}/$ Based on adjusted class a pan data from the class a pan at Wahweap.

TABLE 2 LAKE POWELL EVAPORATION RATE (IN INCHES)

VEAR	HWT	FE1	TAR	APR	TA.	NOT .	Jul	AUG	SEP	00.1	NOV	DEC	TOTAL
1965	2.25	3.62	3.76	4.46	7.29	6.71	6.37	8.57	8.98	59. C89.	3.10	3.53	28. 69
1966	3.24	2.38	3.49	5.06	6.28	8.06	7.70	9.18	6.83	6.12	3.21	5.99	64,54
1967	2.03	1.79	2.86	4.68	5.13	7.00	7.73	7.44	6.75	5.93	3.35	4.13	58.85
1968	2.67	.87	2.72	3.90	6.48	8.79	9.45	10.58	8.66	5.38	5.28	40.4	68.19
1969	1.B6	2.26	2.58	3.92	2.06	7.14	6.B4	7.68	6.73	8.19	4.29	3.31	59.86
1978	36.3	1.54	3.35	4.84	7.76	9.94	10.18	10.97	96.11	7.53	4.94	3.94	78.51
1971	2.13	2.71	3.43	4.78	7.18	7.86	9.81	10.36	11.85	7.22	5.28	4.75	77.28
1972	3,24	2.2	3.75	4.98	5.15	7.71	9.17	9.24	8.02	6.58	5.68	5.18	70.83
1973	3.75	1.75	3.15	4.79	5.64	7.20	B.64	11.02	8.60	6.90	5.70	5.55	. 72.69
1974	3.99	3.28	3.27	÷.	59.5	6.36	8.33	8.41	7.63	4.70	4.24	4.43	64.71
1975	3.54	2.27	3.71	4.66	4.76	6.35	7.23	8.65	7.79	7.81	6.99	4.15	66.26
1976	2.91	2.75	4.26	4.96	4.53	6.93	9.68	19.51	5.70	5.17	4.19	3.89	63.86
1977	2.66	2.64	4.93	4.23	7.48	8.85	12.60	8.01	7.75	6.75	6.84	4.70	76.84
197B	3.05	2.83	3.22	6.59	6.40	7.70	5.42	8.7S	9.05	6.05	7.11	82.9	73.21
1979	4.49	2.55	2.88	4.03	92.5								
MONTHLY	2,98	2.33	3.42	4.56	6.94	7.61	8 . 42	9.24	8.31	6.23	4.94	4.35	AMNUAL MEAN
			; ; ;	(.)	-:" %_);	((r	ر د	:- -		C ((1) -3

Total Pan Evaporation in Inches at Wahweap, Arizona (1962-1975) Table 3

Dec Total							2.69 ^b 108.21	b 2.69 ^b 107.87	b 2.69 ^b 114.26	b 2.69 ^b 113.28	b 2.69 ^b 109.67	2.69 ^b 104.54	2	b 2.69 ^b 96.97	2.69 110.66	
Nov	3.07	3.65	3.90	3.72	4.11	4.37				3.76 ^b	b 3.76 ^b			3.76 ^b	3.76	
0ct	6.82	7.43	9.55	7.49	7.98	8.16	6.99	7.09	7.24	7.11	7.51 ^b	8.05	6.62	7.16	7.51	
Sept	12.21	10.31	13.14	13.06	11.67	10.50	12.76	11.12	12.79	10.98	11.13	11.22	11.30	10.26	11,60	
Aug	18.28	13.90	17.22	16.39	18.13	14.18	12.71	14.88	14.62	15.06	12.67	15.36	14.58	12.79	15.05	
Jul	19.96	20.72	17.96	15.33	18.52	16.41	15.93	15.89	15.78	20.05	16.64	15.43	15.25	15.40	17.08	
Jun	17.36	17.39	16.40	14.36	19.22	15.54	17.41	15.57	17.16	17.42	15.54	15.04	17.07	14.71	16.44	
Мау	15.83	16.17	14.68 ^b	14.54	15.88	13.02	14.63	15.76	16.55	13.77	15.95	13.06	15.41	10.26	14.68	
Apr	12.01	10.38	9.89	8.62	11.96	10.92	9.00	9.74	10.86	10.82	12.16	9.59	10.60	8.32	10.23	Mean
Mar	6.07	6.99	6.25	6.19	7.49	6.51 ^b	6.79	5.97	7.70	6.51 ^b	6.51 ^b	5.15	6.51 ^b	6.51 ^b	6.51	the !
Feb	2.93	3.15	3.03b	3.66	2.11	3.03 ^b	3.03 ^b	3.31	3.03b	3.03b	3.03b	3.03 ^b	3.03 ^b	3.03 ^b	3.03	ars in
Jan	2.08	2.08 ^b	2.08 ^b	2.08 ^b	2.08 ^b	2.08 ^b	2.08 ^D	2.08^{b}	2.08 ^b	2.08 ^b	2.08 ^b	2.08 ^b	2.08 ^b	2.08 ^b	2.08	Number of Years in the Mean
Year	1962	1963	1964	1965	1966	1961	1968	1969	1970	1971	1972	1973	1974	1975	Mean	Numbe

available the mean of the rest of the years for that month was used in calculating the estimated values. Original pan data from U.S. Weather Bureau Climatological Data for Arizona. a = The pan was usually not operated all 12 months of each year. When there was no measurement

Table 4 Evaporation at Lake Powell Based on Adjusted Pan Data from the Class A Pan at Wahweap, Arizona

1			Mal	Apr	Мау	1500	Jul	Aug	Sept	Oct	Nov	Dec	Total
	2.08	2.05	3.04	5.28	5.70	7.99	10.78	11.15	9.04	5.79	4.82	5,38	73.1
1963	2.08 ^b 2.20	2.20	3.50	4.57	5.82	8.00	11.19	8.48	7.63	6.32	5.73	5.38 ^b	70.9
1964	2.08 ^b 2.12 ^b	2.12 ^b	3.12	4.35	5.28 ^b	7.54	9.70	10.50	9.72	8.12	6.12	5.38 ^b	74.03
1965	2.08 ^b	2.56	3.10	3.79	5.23	6.61	8.28	10.00	99.6	6.37		5.38 ^b	68.9
9961	2.08 ^b	1.48	3.74	5.26	5.72	8.84	10.00	11.06	8.64	6.78	6.45	5.38 ^b	75.43
1961	2.08 ^D	2.12^{b}	3.26 ^b	4.80	4.69	7,15	8.86	8.65	7.77	6.94	98.9	5.38 ^b	68.56
1968	2.08 ^D	2.12 ^b	3.40	3.96	5.27	8.01	8.60	7.75	9.44	5.94	6.58	5.38b	68.53
1969	2.08 ^D	2.12	2.98	4.29	2.67	7.16	8.58	9.08	8.23	6.03	9.90°	5.38b	67.5
1970	2.08 ^D	2.12 ^b	3.85	4.78	96.9	7.89	8.52	8.92	9.46	6.15	5.90 ^b	5.38 ^b	71.01
1971	2.08 ^D	2.12 ^b		4.76	4.96	8.01	10.83	9.91	8.12	6.04	2.90 ^b	5.38 ^b	70.64
1972	2.08 ^b	2.12 ^b		5.35	5.74	7.15	8.99	7.73	8.24	6.38 ^b	5	5.38 ^b	68.31
1973	2.08 ^b	2.12 ^b	2.58	4.22	4.70	6.92	8.33	9.37	8.30	6.84	6.03	5.38 ^b	66.87
1974	$2.08^{\rm b}$	2.12 ^b	3.25 ^b	4.66	5.55	7.85	8.24	8.89	8,36	5.63	4.74	5.38 ^b	66.75
1975	2.08 ⁵	2.12 ^b	3.25 ^b	3.66	3.69	6.77	8.32	7.80	7.59	60.9	5.90 ^b	5.38 ^b	62.56
Monthly Mean 2.	80	2.12	3.26	4.50	5.28	7.56	9.22	9.18	8.58	6.38	5.90	Annua 5.38	Annual Mean 38 69.44

surement available the mean of the rest of the years for that month was used in calculating the adjusted values. Original pan data from U.S. Weather Bureau Climatological Data for Arizona." a = The pan was usually not operated all 12 months of each year. When there was no mea-

b = Based on estimated values as per note a above.

TABLE 5 LAKE POWELL GROSS EVAPORATION (IN ACRE-FEET)

YEAR	JAH	FE3	MAR	APR	MAY	JCH.	JUL	PUG	9£P	00.1	¥0x	DEC	TOTAL
1965	6526	13693	16284	19347	31686	34226	33546	47651	49688	15586	17092	19755	303107
1966	18316	13374	19643	29179	1401	48336	45478	52326	37846	33069	17085	15674	367333
1961	7905	2692	14140	28522	24148	35897	45769	41102	36725	32060	18128	22215	305267
1968	11097	46 21	14329	19661	32754	\$9258	57105	50575	52410	32170	31154	23525	379559
1969	10793	13236	15347	23801	33655	51280	50463	28835	47867	58190	30604	23343	414474
1978	16457	18673	53484	27846	54727	78263	8 1000	89867	97444	61516	40656	32436	6 17279
1971	17389	225 46	28497	39152	64953	70200	90432	94118	105832	63966	46528	41367	616089
	27913	18958	32798	42856	44672	69462	82964	81999	68649	55809	49077	44464	618961
1973	31424	14389	25891	37907	47439	68525	61088	114360	97898	80503	72203	5B+93	137051
	5861+	34630	34846	47623	62652	73154	95474	94845	82829	50314	45177	46768	769489
1975	37839	23706	38782	41864	50718	72126	86256	103092	91344	56572	69379	4B 1 46	752644
1976	33714	31736	48814	98293	52025	81437	80869	99529	65551	58625	46787	42763	65869
1977	26882	28362	52722	45565	86915	76212	98286	83545	78142	66994	67540	1865*	753367
1978	28939	27012	29830	58941	61763	19261	69854	95946	92911	61869	71042	61838	734293
1979	43360	23997	27972	46820	61829								
MONTHLY	24331	19195	28217	36923	4919B	63184	71790	78555	71789	54277	44468	37621	

reservoir did not exist. For this study the evapotranspiration that must be subtracted was determined in four parts.

EVAPORATION FROM THE PRE-RESERVOIR WATER SURFACE

The first part was the evaporation from the pre-reservoir river water surface. It is computed by multiplying the area of the river by the gross evaporation rate. The river water surface area was determined using the following criteria.

- (1) The aerial photographs from which the Lake Powell topography came were flown in September and October of 1958 and 1959 when the river was at a very low stage.
- a very low stage.

 (2) The average flow of the river over the period of record was about 18,000 c.f.s. at Lees Ferry.
- (3) Tail water curves taken in the vicinity of Glen Canyon Dam indicate a rise of only about 5 feet for an increase in flow of 15,000 c.f.s.
- (4) Since the water line shown on the topography represents a flow of about 6,000 c.f.s., it was assumed that the contour closest to this water line would represent average flow conditions.
- (5) Where a contour crossed the river on a given topography sheet, a line representing the average flow line was drawn in and the area planimetered accordingly.
- (6) Sandbars that did not show vegetation were assumed to be included in the water surface area at 18,000 c.f.s. average flow.

The river-elevation relationship is shown in Figure 4. The gross evaporation rate from Table 4 was used. The resulting river evaporation is shown in Table 8 Column 2.

STREAMSIDE EVAPOTRANSPIRATION

The second part was the evapotranspiration that would have occurred from the vegetation, which is mostly phreatophyte, and evaporation from the wetted soil on the streambank if the reservoir did not exist. It was computed by multiplying the evapotranspiration rate by the streamside area. The evapotranspiration rate was computed by the Blaney – Criddle method $\frac{7}{4}$ as shown in Table 7 and described below. The streamside areas were determined under a contract between the University of Utah and the Bureau of Reclamation in the late 1950's before Lake Powell started to fill $\frac{9}{4}$. The vegetation density was measured along transects. These were used as an index to make ocular estimates of the remaining areas. The areas were measured by planimeter from maps which were prepared from overlay maps and tabular data from the field. The area-elevation relationship is shown in Figure 5. The main source of water for this part is from percolation with a small contribution from precipitation. The streamside evapotranspiration is shown in Table 8 Column 3.

FIGURE 4

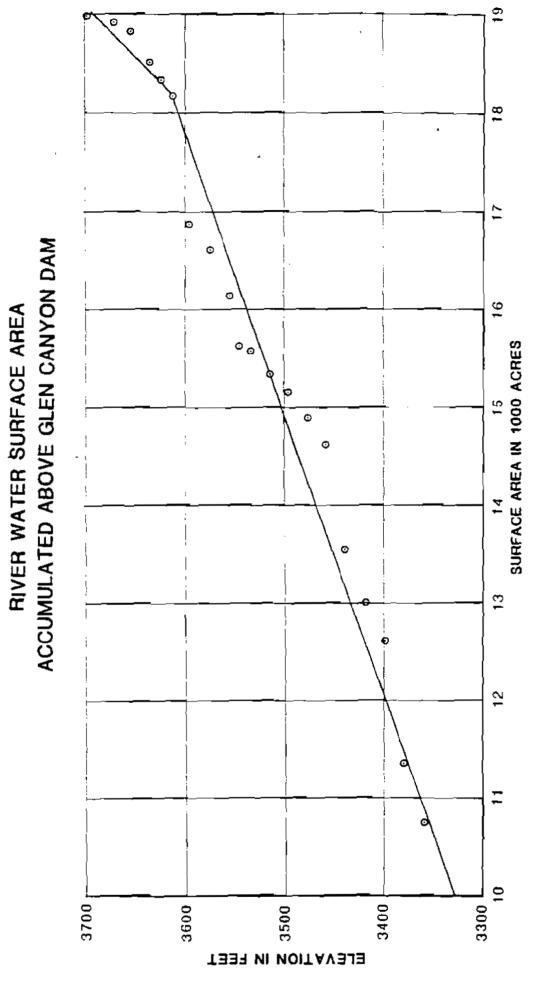


FIGURE 5

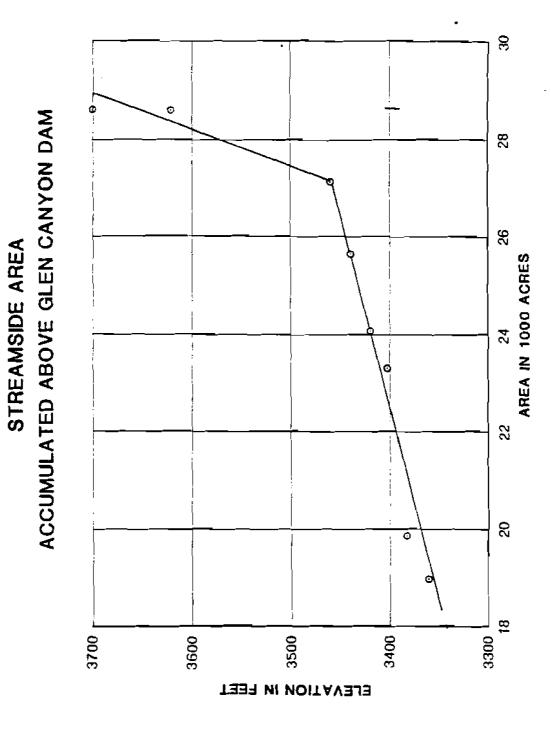
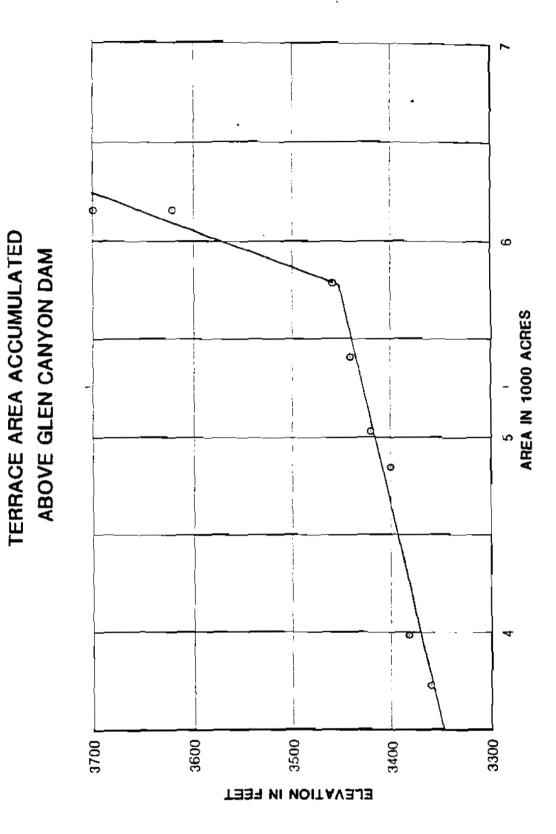


FIGURE 6



TERRACE EVAPOTRANSPIRATION

The third part is the evapotranspiration from the terrace areas under prereservoir conditions. It was computed by multiplying the evapotranspiration rate by the terrace area. The evapotranspiration rate was determined by the Blaney-Criddle method 7/ described below. The areas were determined by the same survey referred to above. This water reaches the root zone mostly by capillary action with some by precipitation. The terrace area-elevation curve is shown in Figure 6. The resulting evapotranspiration is shown in Table 8 Column 4.

BLANEY-CRIDDLE METHOD

The Blaney-Criddle method of computing evapotranspiration (consumptive-use) was chosen because of the minimal data requirements and accuracy acceptable for this purpose. The basic equation is:

u=fk

Where u is the evapotranspiration rate in inches. k is an emperical coeffecient dependent on the type of vegetation. Consumptive use coefficients have been determined mostly for irrigated crops so there has been little investigation of native vegetation.

From values given for k by Blaney 10/ for native vegetation for several densities of vegetation 1.1 was selected for the streamside area and 0.9 was used for the terrace area. The variable f is calculated as (t)(p)/100. Where t is the mean monthly air temperature in degrees farenheit and p is the monthly percent of annual daylight hours and is dependent upon the latitude. 39° north latitude was used. Therefore u=(t)x(p)x(k)/100. Table 6 shows the computation of (p)x(k)/100 for the streamside area and the terrace area. This was multiplied by the average temperature for the month to obtain the evapotranspiration rates.

EVAPOTRANSPIRATION OF REMAINING AREAS

The fourth part is the evapotranspiration from the remaining area of the reservoir under pre-reservoir condition.

Most of the precipitation falling on the area of Lake Powell would not have produced runoff because it would have evaporated from the vegetation and soil or it would have transpired from the vegetation. In consumptive use studies this is termed effective precipitation. It does not include precipitation that causes runoff. The method of determining the effective precipitation used is described in a report by R. A. Schleusener 8/. The precipitation was computed from seven stations: Page, Wahweap, Bullfrog, Canyonlands, Hite, Mexican Hut, and Natural bridges. Since each of these stations were located above the maximum elevation of Lake Powell, and since precipitation increases with elevation, it was necessary to reduce the precipitation to an equivalent for Lake Powell at a representative elevation of 3,600 feet. This was done by plotting the average annual precipitation for 1963 through 1980 against the elevation for the seven stations and drawing a curve throught the points. The resulting average annual precipitation from this curve is 6.33 inches. The ratio of 6.33 to the average annual precipitation at each station was multiplied by the monthly precipi-

TABLE 6
BLANEY-CRIDDLE
COMPUTATION OF p x k
100

		Str	reamside	Ter	race
	<u>%</u>	κ	p x k 100	K	p x k
January	6.92	1.1	.0761	0.9	.0623
February	6.87	1.1	.0756	0.9	.0618
March	8.34	1.1	.0917	0.9	.075
April	8.87	1.1	.0975	0.9	.0798
May	9.85	1.1	.1083	0.9	.0886
June	9.89	1.1	.1088	0.9	.089
July	10.05	1.1	.1105	0.9	.0904
August	9.44	1.1	.1034	0.9	.085
September	8.37	1.1	.0921	0.9	.0829
October	7.83	1,1	.0861	0.9	.0775
November	6.88	1.1	.0757	0.9	.0681
December	6.69	1.1	.0736	0.9	.0621
Total	100.00				

tation to reduce it to the equivalent precipitation at 3,600 feet. The equivalent precipitation for all stations was then totaled and divided by the number of stations on a monthly basis. Table 6 was adapted from the report by R. A. Schleusener 8/.

TABLE 7
Effective Precipitation in Inches

Month Jan Feb Mar April May June July Aug Sept Oct Nov Dec .6 .6 .8 .8 .8 .8 1.0 1.0 1.0 .8 .8 .8

The precipitation up to the limit shown in Table 7 was multiplied by the remaining area. This is shown as column 5 in Table 8. The remaining area is the total area of the reservoir for the month minus the total of the water surface area, the streamside area, and the terrace area. From these computations it was determined that about 95 percent of the precipitation on the reservoir area would have evaporated and transpired.

RESULTS

Table 8 shows the computed monthly evaporation for each of the four parts and the resulting net evaporation for the period January 1965 through May 1979.

Table 9 shows the net annual evaporation, as described under PROCEDURE, which has previously been used on a preliminary basis, compared to the net annual evaporation computed from this study (Table 8). The net evaporation is less under this study when the reservoir is low but greater when the reservoir is high. The average evaporation under this study is 5 percent higher than the preliminary figures. This is mostly due to the 3 percent higher gross evaporation rate of 68.3 inches per year compared to 66.2 inches from the former estimates.

RECOMMENDATIONS

It is recommended that the results of this study be used to make a water budget analysis for Lake Powell. This will improve the estimate of the amount of water stored in the banks. It might also help to determine the amount of bank storage that is recoverable.

It is also recommended that the results of this study be used to determine a simpler method of estimating evaporation. A method that could be used in operations would be beneficial. One method that should be considered is to use pan evaporation at Wahweap.

T.... 8 LAKE POWELL NET EVAPORATION (IN ACRE-FEET)

(7) (1-6) NET EVAPORATION	3600 0000 0000 0000 0000 0000 0000 0000	162262	######################################	218670	2000 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	158006
(6) (2+3+4+5) fotal Abjustnent	66 66 66 66 66 66 66 66 66 66 66 66 66	146621	66 44 44 44 44 44 44 44 44 44 44 44 44 4	148663		151117
(5) EWPO- TRANSPIRATION FROM REMAINING AREA	4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	12964	######################################	16933	1100011 U U U U U U U U U U U U U U U U	24384
EVAPO- TRANSPIRATION FROM TERRACE	1168 1768 1768 1769 1769 1769 1769 1769 1769 1769 1769	35967	1300 1300 1300 1300 1300 1300 1300 1300	37081	137 200 200 200 200 200 200 200 200 200 20	36910
(3) EVAPORATION FROM STREAMSINE		14750	20000000000000000000000000000000000000	15325	255 1100 1100 1100 1100 1100 1100 1100 1	14828
(2) EVAPORATION FROM RIVER	8887278 8887278 8887278 8887278 88874 87674 87674 8764 8764	17060	4276 4694 6717 6717 16827 1218 1218 1759 159 159	85324	25.59 26.73 26.73 29.73 29.73 26.13 26.13 26.13 26.13 26.13 26.13 26.13 26.13	75895
(1) GROSS EUMPORATION	9753 13693 19624 39626 39626 33322 47651 175586 175983 175586	362883	18315 19315 19843 139179 139136 13969 17965 17685	367333	1 8 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9	369123
MO. OF		R TOTALS:	สลิสลิสลิสลิสลิส	R TOTALS!		R TOTALS
VENE MENTH	22 - 22 - 22 - 22 - 22 - 22 - 22 - 22	CALENDER YEAR	1966 1966 1966 1966 1966 1966 1966 1966	CALENDER YEAR	1967 1967 1967 1967 1967 1967 1967 1967	CALEMBER YEAR

TABLE 8 LAKE POWELL NET EVAPORATION (IN ACRE-FEET)

(2)	EUAPORATION	a = a = a a a a a a a a a a	222478		261138	10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050 10050	436190
(9)	TOTAL JUSTINE	4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.05 C 4.	157081		153336		187179
(2)	EUAPO- TRANSPIRATION FROM REMAINING AREA	23.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00 20.00	17027	0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.100 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000	17844	480-00.42 480-00.42 480-00.42 680-00.00 680-00.00 680-00.00 680-00.00	20056
(+)	EVAPO- TRANSPIRATION FROM TERRACE	01100000000000000000000000000000000000	35043	######################################	37017		37262
Ĉ	EUMPORMION FROM STREMMSIDE	**************************************	14492	68999999999999999999999999999999999999	15431	######################################	15626
(2)	EURPORATION FROM RIVER	268 1169 4951 1166 1166 1166 720 720 720 720 720 730 730 730 730 730 730 730 730 730 73	90519	24773 2455 2455 26772 2772 2772 2772 2772 2666 6666	83844	2000 2000 2000 2000 2000 2000 2000 200	114235
(1)	GROSS EUAPORATION	######################################	979559		414424	24000000000000000000000000000000000000	617279
	MG. OF DAYS	ក៏ដីកើតិកិតិកិតិកិ តិ	TOTALS		TOTALS		TOTALS:
	VEAR. BONTH		NDER YEAR	→ 0000-000-000-000-000-000-000-000-000-0	ER YEAR	このですらなっている。	ER YEAR
	VESS		CALEND		CALENDER		CALENDER

TABLE 8 LAKE POWELL NET EVAPORATION (IN ACRE-FEET)

£ 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5 5	EVAPORATION	######################################	484442	**************************************	430764	######################################	546361
(6) (2+3+4+5)	POTAL		209347		187297		199690
(5)	EVAPO- TRANSPIRATION FROM REMAINING AREA		37654	180 190 190 190 190 190 190 190 190 190 19	26759	424400 424400 44460 44660 44660 44660 44660 44660 44660 44660 44660 44660 44660 44660 44660 44660 44660 44660 44660 44660 44660 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44600 44000 44000 44000 44000 44000 44000 44000 44000 44000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 46000 4600	27009
(4)	TRANSPIRATION FROM TERRACE ACRE-FEET	1149 2472 2472 2472 2472 2472 2472 2472 24	37331	1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1 1	38131	10000000000000000000000000000000000000	37362
(3)	EURPURATION FROM STREAMSIDE	20000000000000000000000000000000000000	15751	6 1 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2	16072	200 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	15826
(2)	EUMPOKATION FROM RIVER	4525 4878 6963 11875 11793 10896 17855 17855	118611	4846 3392 5634 7366 111664 11369 11999 11999 1793 7793	166335	5562 2584 2581 13869 13869 13869 11866 11868 1188	110553
(1)	GROSS EVAPORATION	25113 27113 28162 29157 569157 569157 536118 63966 1556	683789	22 182 182 182 182 183 183 183 183 183 183 183 183 183 183	618061	31424 14389 255891 37267 4739 88619 17496 97498 96593 72203	737851
;	MD. OF	######################################	TOTALS	កសិកិសិកភិសិកភិសិក	TOTALS!		TOTALS
1	VEAR. MONTH		DER YEAR		DER VEAR	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	NDER VEAR
	YEAR	555555555555555555555555555555555555555	CALENDER	20000000000000000000000000000000000000	CALENDER	1873 1873 1873 1873 1873 1873 1873 1873	CALEN

TAB. LAKE POWELL NE! EVAPORATION (IN ACRE-FEET)

(7)	EUAPORATION	10000000000000000000000000000000000000	518441	######################################	556956	00000000000000000000000000000000000000	513705
(6) (2+3+4+5)	₹ :	######################################	189609	タンは ちゅうしゅうしゃ	196588		184892
(2)	EUAPO- TRANSPIRATION FROM MEMAINING AREA	167 167 237 237 3239 6661 6375 6575	36222	4 00000 4 000000 1 000000 1 000000 1 000000 1 000000	10194	551 124 125 125 125 125 125 125 125 125 125 125	12506
§	EVAPO- TRANSPIRATION FROM TERRACE	10000000000000000000000000000000000000	37385	######################################	37397		38459
(3)	EUAPORATION FROM STREAMSIDE	11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00 11.00	15932	7.8.11.8.11.8.11.8.12.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.13.14.14.13.14.14.13.14.14.14.14.14.14.14.14.14.14.14.14.14.	15926		16394
(8)		65111 6510 6510 6510 6510 6510 6510 6510	100070	4	163671	45 45 45 45 45 45 45 45 45 45 45 45 45 4	99518
3	GR05S VAPORATI	4	9508⊕2	93-93-93-93-93-93-93-93-93-93-93-93-93-9	752644	463444	698597
	NO. OF DAYS		R TOTALS:		R TOTALS	កលិកគិតគិតគិតគិត	R TOTALS
	ножи		KER YEAR		KER YEAR		DER YEAR
	YEAR		CALENDER	<u>ខេត្តបានធ្វាធិប្បក្សិសិសិសិសិសិសិសិសិសិសិសិសិសិសិសិសិសិសិ</u>	CALENDER	1976 1976 1976 1976 1976 1976 1976	CALENDER

TABLE 8 LAKE POWELL NET EVAPORATION (IN ACRE-FEET)

	* •					
(2) (4-6)	EUAPORATION	S-LUNNARRRRRR BC-LUC P44 LURRRR URBRA-BLURRRR F-SURB-LUNRRRR BURRRURRRA-BRA BURRRURRRA-BRA BURRRURRRA-BRA BURRRURRRA-BA	537366	500 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	540504	300 100 100 100 100 100 100 100 100 100
(6)	TOTAL		216061	7.111111111111111111111111111111111111	193789	16947 7498 9286 11556 16543
(§)	EVAPO- TRANSPIRATION FROM REMAINING AREA	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	41467	24.00 SS SS SS SS SS SS SS SS SS SS SS SS S	86898	287.587.586.787.787.787.787.787.986.986.986.986.986.986.986.986.986.986
\$	EUAPO- TRANSPIRATION FROM TERRACE	1868 2663 3663 4857 8233 4856 1896 1656	39458	186 34 34 133 133 133 133 133 133 133 133 1	38382	1560 2003 3004 3738 4676
(3)	EUAPORATION FROM STREAMSIDE		16752	20000000000000000000000000000000000000	16229	621 1259 1555 1944
(8)	EUGPORATION FROM RIVER	4414 4414 4414 655 655 655 655 655 655 655 655 655 65	118384	4648 4395 4891 9571 1838 1954 1354 1354 16896 9588	112240	6854 3846 4399 6186 8913
(1	GROSS EURPORATION	200	753367	62 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	734293	43360 23997 27972 40820 62819
	HO. OF DAYS	ਜ਼ਜ਼ਜ਼ਜ਼ਜ਼ਜ਼ਜ਼ਜ਼ਜ਼ਜ਼ ਜ਼ਜ਼ਜ਼	TOTALS:	~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~~	TOTALS!	######################################
	HOHETH		ER YEAR	→さらすららて B なる → ご	YER YEAR	−007
	VE R	10000000000000000000000000000000000000	CALENDER	11090908 11090909 11090908 11090908 11090908 11090908	CALENDER	1979 1979 1979 1979 1979

TABLE 9
LAKE POWELL NET EVAPORATION
1,000 ACRE-FEET

Calendar Year	Preliminary* <pre>Net Evaporation</pre>	Net Evaporation This Study
1965	200	162
1966	236	219
1967	215	158
1968	237	222
1969	300	261
1970	348	430
1971	398	484
1972	392	431
1973	441	546
1974	512	518
1975	523	556
1976	544	514
1977	486	537
1978	<u>464</u>	<u>541</u>
Total	5,296	5,579
Average	378	398

^{*} Computed from pan evaporation rate as described under PROCEDURE.

REFERENCES

- 1. U.S. Geological Survey, 1954a, <u>Water-Loss Investigations</u>: <u>Lake Hefner Studies</u>, <u>Technical Report</u>: U.S. Geol. Survey Prof. Paper 269. Previously published as U.S. Geol. Survey Circ. 229 (1952) and as U.S. Navy Electronics Laboratory Report 327.
- 2. U.S. Geological Survey, 1954b, <u>Water-Loss Investigations</u>: <u>Lake Hefner Studies</u>, <u>Base Data Report</u>: U.S. Geol. Survey Prof. Paper 270; also published as U.S. Navy Electronics Laboratory Report 328.
- 3. NOAA Technical Report NWS33, 1959, "Evaporation Atlas for the Contiguous 48 States" Dept. of Comm. NWS, June 1982.
- 4. Harbeck et al. U.S. Geological Survey, 1958, <u>Water Loss Investigations</u>: <u>Lake Mead Studies</u>, Professional Paper Number 298.
- 5. Jacoby, Gordon C. Jr., et al. 1977, <u>Lake Powel Research Project Bulletin</u>, <u>Number 48</u>, National Science Foundation Institute of Geophysics and Planetary Physics University of California, Los Angeles.
- 6. G. Earl Harbeck, Jr., U.S. Geological Survey, 1962, <u>A Practice Field</u> Technique for Measuring Reservoir Evaporation Utilizing Mass-Transfer Theory, U.S.G.S. Professional Paper No. 272-E.
- 7. Blaney, H.F., Criddle, W. D., 1962, <u>Determining Consumptive Use and Irrigation Water Requirements</u>, U.S. Department of Agriculture Tech. Bulletin 1275.
- 8. Schleusener, R.A., Crow, L.W., 1961, Analysis of Precipitation Data in the Upper Colorado River Basin, Colorado State University.
- 9. Woodbury, A. M., Durrant S. D., Flowers, S., 1959, <u>A Survey of Vegetation</u> in the Glen Canyon Reservoir Basin Anthropological Papers Number 36, University of Utah Press.
- 10. Blaney H. F., Criddle, 1948, <u>Final Report Engineering Advisory Committee</u> to Upper Colorado River Basin Compact Commissi<u>on</u>.
- 11. Jensen, M.E., Editor, 1973, <u>Consumptive Use of Water and Irrigation Water</u> <u>Requirements</u>, American Society of Civil Engineers.